



Influence of Large-scale PV on Voltage Stability of Sub-transmission System

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Abstract: Voltage instability is considered as one of the main threats to secure operation of power systems around the world. Grid connected renewable energy-based generation are deploying in recent years for many economic and environmental reasons. This type of generation could have significant impact on power system voltage stability given the nature of the primary source for generation and the technology used for energy conversion. This paper presents the results of an investigation of static voltage stability in heavily stressed IEEE-14 bus test system with large-scale PV integration. The study focused on the impact of large-scale PV penetrations and dynamic VAR placements on voltage stability of the sub-transmission system. For this study, the test system loads are modeled as the summer peak load of a realistic system. The comparison of STATCOM and SVC performance with large-scale PV is also discussed.

Keywords: PV generator, STATCOM, SVC, trajectory sensitivity index, voltage stability.

1. Introduction

Utilization of renewable energy comes from the perspective of environmental conservation and fossil fuel shortage. Recent studies suggest that in medium and long terms, photovoltaic (PV) generator will become commercially so attractive that large-scale implementation of this type can be seen in many parts of the world [1], [2]. A large-scale PV generation system includes photovoltaic array, maximum power point tracking (MPPT), DC/AC converter and the associated controllers. It is a multivariable and non-linear system, and its performance depends on environmental conditions. Recently, the increasing penetration levels of PV plants are raising concerns to utilities due to possible negative impacts on power system stability as speculated by a number of studies [3]-[5]. Thus, the thorough investigation of power system stability with large-scale PV is an urgent task.

Among stability issues, voltage instability has been a major concern for power system. Several major power interruptions have been linked to power system voltage instability in recent past [6], [7]. It has been proved that inadequate reactive power compensation during stressed operating condition can lead to voltage instability. Although large-scale PV is capable of generating reactive power, however, the operation of PV in terminal voltage mode has the potential for adverse interaction with other voltage controllers [8]. Therefore, grid code requires operation at power factors equal or greater than 0.95 for PV generators [9], [10]. Moreover, the size and position of large-scale PV generator can introduce detrimental effect on power system voltage stability as the level of PV penetration increased.

Furthermore, the technical regulations or specific standards are trying to shape the conventional control strategies to allow the flawless integration of renewable energy based distributed generation (DG) in main grid. According to technical regulations or standards the post fault voltage recovery time at DG bus is crucial as it requires DG to trip, if recovery time exceeds certain limits [9], [10]. With increased penetration of renewable energy DG, early

tripping of DG due to local disturbance can further risk the stability of the system. Hence system operator becomes responsible to maintain the voltage profile under all operating conditions. As a result, fault tolerant control algorithm based on dynamic VAR planning (e.g. placement of FACTS) is applied in DG integrated system. The most common, or preferred, dynamic VAR planning with multiple DGs is the placement of dynamic VAR device at the point of common coupling of DG.

In this paper, the result of static voltage stability with large-scale PV penetrations on sub-transmission system for realistic load composition is presented. Three dynamic VAR placements algorithms are compared in terms of long-term voltage stability with large-scale PV penetrations. The impact of SVC and STATCOM placement on static voltage stability is studied, and their performances are compared.

The rest of the paper is organised as follows. Section II presents the methodologies used for static voltage stability analysis followed by the underlying concept of trajectory sensitivity index. Modelling of PV and dynamic VAR compensators are illustrated in Section III. Section IV briefly introduces the test system and its composition. Study results based on IEEE-14 bus test system are presented in Section V. Section VI gives the relevant conclusions.

2. Methodology

A. Q-V Modal Analysis

The analytical description of a power system applicable to stability study is given by the following differential-algebraic equation [11]

$$\dot{x} = f(x, y, \lambda) \quad (1)$$

$$0 = g(x, y, \lambda) \quad (2)$$

where, $x \in \mathfrak{R}^n$ is a vector of state variables; $y \in \mathfrak{R}^m$ is a vector of algebraic variables (e.g., load voltage phasor magnitude and angles); $\lambda \in \mathfrak{R}^l$ is a set of uncontrollable phasor magnitude such as variation of active and reactive power of loads. The set of system algebraic equations can be expressed as follows:

$$\begin{bmatrix} \Delta P \\ \Delta Q \end{bmatrix} = \begin{bmatrix} \frac{\partial P}{\partial \theta} & \frac{\partial P}{\partial V} \\ \frac{\partial Q}{\partial \theta} & \frac{\partial Q}{\partial V} \end{bmatrix} \begin{bmatrix} \Delta \theta \\ \Delta V \end{bmatrix} \quad (3)$$

where, ΔP , ΔQ are mismatch power vectors. ΔV , $\Delta \theta$ are unknown voltage magnitude and angle correction vectors.

For steady state voltage stability analysis, the change of active power is considered as constant (zero) in power flow Jacobian. After some manipulation, from eq. (3) we can get the reduced Jacobian (J_R) as

$$J_R = \xi_{n \times n} \Lambda_{n \times n} \eta_{n \times n} \quad (4)$$

where, ξ = matrix of right eigenvectors corresponding to all eigenvalue of the system, Λ = diagonal matrix of system eigenvalues and η = matrix of left eigenvectors corresponding to all eigenvalues of the system. By using (4) expression for modal voltage and modal reactive power variations corresponding to i^{th} eigenvalue can be obtained,

$$v_i = \lambda_i^{-1} q_i \quad (5)$$

system. Sensitivity of i^{th} bus voltage (V) with respect to reactive power (Q) injection at j^{th} bus can be calculated as $\frac{\partial v_i}{\partial Q_j}$. Then the trajectory sensitivity index proposed in [15] is defined as

$$TSI_j = \sum_{k=1}^{N_k} w_k \left[\sum_{i=1}^n w_{bi} \left[\frac{\partial v_i}{\partial Q_j} \right]_{t=t_k} \right] \quad (13)$$

where, w_{bi} is the weighting factor to represent the importance of i^{th} bus on the sensitivity and w_{bi} has been chosen to be 1 for all the load buses and the buses with PV generators. w_k is the weighting factor to designate the importance of time instant k . Higher value of w_k is selected for the time instants just after the fault. Bus with higher trajectory sensitivity index is the the best location for dynamic VAR placement with multiple PVs.

3. PV Generator and Dynamic Var Compensator Modelling Overview

A. PV Generator Modelling Overview

For large-scale operation of PV, modules are connected in series and parallel to form an array. The array output current equation can be derived from the basic solar cell output current equation and can be expressed as [16]

$$I_{PV} = I_{SCA}(G) - N_P \times I_0 \left[e^{\frac{(V_A + I_{PV} R_s)q}{nN_S kT}} - 1 \right] \quad (14)$$

where, I_{PV} = array current (A), V_A = array voltage (V), q = electron charge (1.6×10^{-19} C), k = Boltzmann's constant (1.38×10^{-19}), n = ideal factor, T = ambient temperature, I_0 = diode reverse saturation current (A), R_s = array series resistance (Ω), $I_{SCA}(G) = N_p I_{SC}(G)$, $N_S = N_{CS} N_{SM}$, $N_P = N_{SP}$, N_{SM} and N_{SP} represent the number of modules connected in series and parallel in the photovoltaic array, respectively, N_{CS} = number of series connected cells in a module, I_{SC} = cell short circuit current (A) and G = solar insolation at any instant (W/m^2).

DC power generated from PV array is considered to be the real power injected into the network. Real and reactive power generation from the PV system is controlled by voltage source converter. For proper analysis, three-phase inverter terminal voltage is converted into d-q axis voltage component (Park's voltages). Park's voltages are related to the PV array terminal voltage by following relationship [17]:

$$\begin{cases} V_d = \frac{\sqrt{3}mV_A}{2\sqrt{2}} \cos \delta \\ V_q = -\frac{\sqrt{3}mV_A}{2\sqrt{2}} \sin \delta \end{cases} \quad (15)$$

where, m is modulation index (0,1), δ is the phase angle ($\pm\pi/2, 0$) and V_A represents PV array terminal voltage. Let us assume that the DC power generated by the PV array is delivered to the network, then

$$P_{dc} = P_{ac} = \frac{0.6128 m V_A V_s \sin \delta}{X_t} \quad (16)$$

and, the reactive power equation of the PV generator can be represented as

4. Test System and its Composition

A. Test System

On-line diagram of IEEE-14 bus test system is depicted in Figure 3. In original test system, there are five synchronous generators among which three of them are synchronous compensators used only for reactive power support, and two generators are located at buses 1 and 2 [18]. There are twenty branches and fourteen buses with eleven load buses. For this study, a slightly modified IEEE-14 bus system is considered. The modification from original IEEE-14 bus system is that generators located at buses 3 and 6 are changed from synchronous compensators to synchronous generators and the loading of the system are increased to 362.5 MW and 108.5 MVar, respectively. Results included in this paper are obtained by using MATLAB and MATLAB based power system analysis software known as PSAT [20].

B. Load Composition

Proper modelling of loads for power system static voltage stability study is important as they have profound impact on voltage stability. Utilities break their loads into various compositions with presence of different percentages of loads. For this study, loads are modeled as the summer peak load of a realistic system. The active part of the load is modeled as 100 % constant current and reactive part of the load is modeled as 100 % constant impedance load [21].

PV Generation and It Size

An aggregated PV generator depicted in Figure 4 is used for the analysis. A 10 MVA PV generator is considered for the initial analysis; while for the investigation of the penetration effect of PV on static voltage stability, PV generator size is increased by 10 MVA step size. Aggregated PV generator data are taken from [12].

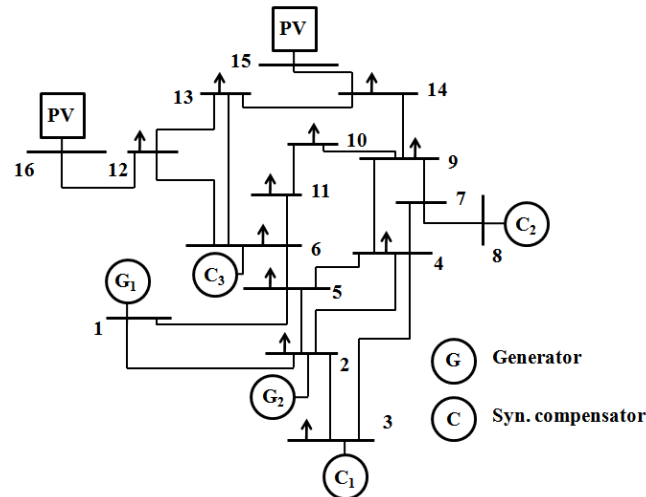


Figure 3. Single-line diagram of IEEE-14 bus test system.

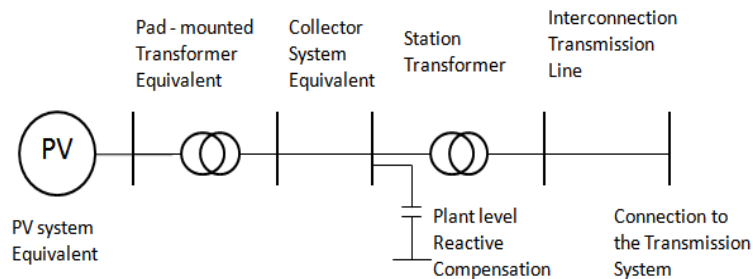


Figure 4. Schematic diagram of an aggregated PV generator.

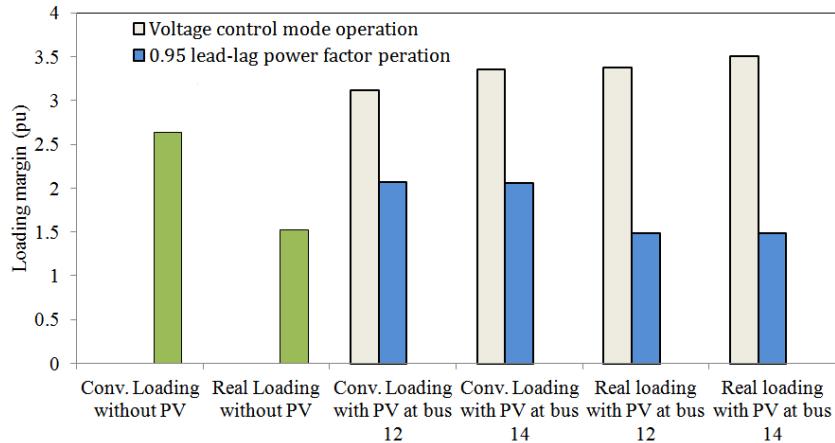


Figure 5. Loading margins for different loading directions (with and without PV).

In case of contingencies, the system characteristics have changed. Effect of PV generator penetration on system voltage stability during contingency is analyzed by the outage of line **1-5**. Table III illustrates the effect of PV locations on system critical eigenvalue for normal and N-1 contingency. Critical eigenvalue of the system at the base case for this particular N-1 contingency is **2.5658**. From Table III it can be observed that for all PV locations critical eigenvalue of the system is higher than the base case at normal operating condition, while during N-1 contingency degree of stability is less than the base case for voltage control mode operated PV at bus 12. From the table it is also noticeable that for all PV locations critical eigenvalue of the system for normal and N-1 contingency is lower than the system base case when integrated PV operated at power factor control mode. From the table, it is worthwhile to note that for voltage control mode operation in most of the cases dispersed PV location improves the degree of voltage stability.

Table 3. Impact of PV Locations on Critical Eigenvalue

PV location bus	Critical eigenvalue (Voltage control mode operation of PV)		Critical eigenvalue (Power factor operation of PV)	
	Normal	N-1 contingency	Normal	N-1 contingency
12	2.6697	2.4025	1.5756	1.5669
13	2.6898	2.6091	2.2618	2.2516
14	3.9398	3.6791	2.3525	2.3315
10,12	4.5266	4.4966	1.775	1.7572
9,13	6.4356	6.4346	1.8595	1.8376
5,14	3.9046	3.8876	1.5683	1.555

B. Effect of PV Penetration

To study the impact of increased PV penetration on voltage stability, the following scenarios are considered,

1. Concentrated PV penetration.
2. Dispersed PV penetration.

Figure 6 shows the effect of concentrated PV penetration on the degree of system stability. From the figure it can be seen that for all the buses increased PV penetration does not have positive impact on system stability. At some location (**e.g., bus 12**), penetration of PV does not appear to contribute to the voltage stability of the system; meanwhile other position (**bus 9**) has both positive and negative impact on voltage stability with incremental penetration. It can be

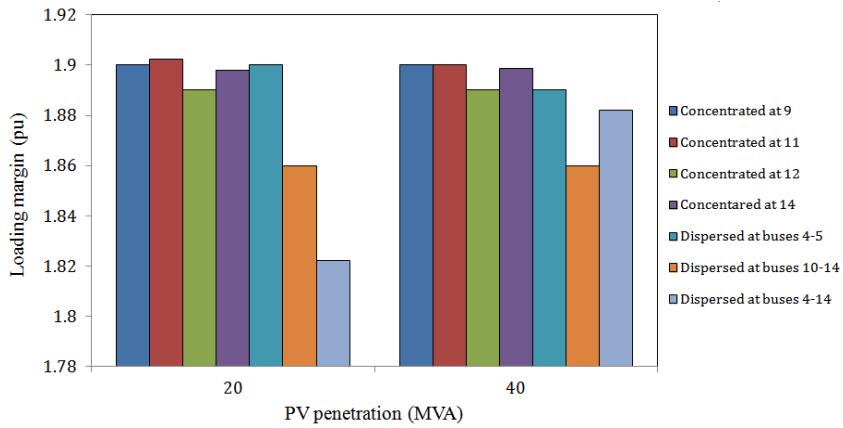


Figure 8. Loading margins for concentrated and dispersed PV penetrations.

C. Location of Dynamic VAr Compensator

For this study PV generators are integrated at buses **12 and 14**, respectively. Three scenarios have been considered to study the effect of dynamic VAr compensator placement on system static voltage stability performance with large-scale PV. These are as follows;

1. Dynamic VAr compensator at each PV generator bus.
2. Dynamic compensator at the weakest bus of the system.
3. Dynamic compensator placed at the bus with highest TSI.

From bus participation factor analysis at stressed condition corresponding to critical eigenvalue reveals that **bus 14** is the weakest bus of the system. Figure 9 displays the trajectory sensitivity index (TSI) of the buses in area-2. TSI is highest for **bus 9**, which is located in the zone where PV generators are integrated to the system. Comparison of system loading margins for STATCOM placements are shown in Figure 10. From Figure 10 it can be seen that system loading margin is highest for TSI based STATCOM placement as compared to STATCOM placement at the weakest bus, and at the point of common coupling of PV generator.

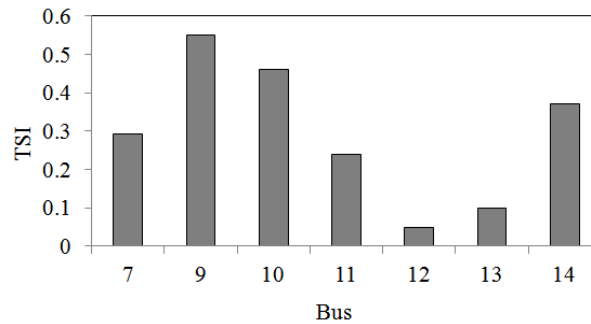


Figure 9. Trajectory sensitivity index values for the buses in area-2.

From results in Figure 10 it can be observed that placement of STATCOM at the weakest bus of the system provides slightly better system loading margin than system without PV, with PV and STATCOM at each PV bus.

- STATCOM provides better option to enhance static voltage stability margin of the system with large-scale PVs.
- Placement of SVCs in PV generator buses are found to be more effective in enhancing voltage stability margin rather than the weakest bus placement or the placement based on short term dynamic VAr support.

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